

MODELING AND SIMULATION OF WWTP

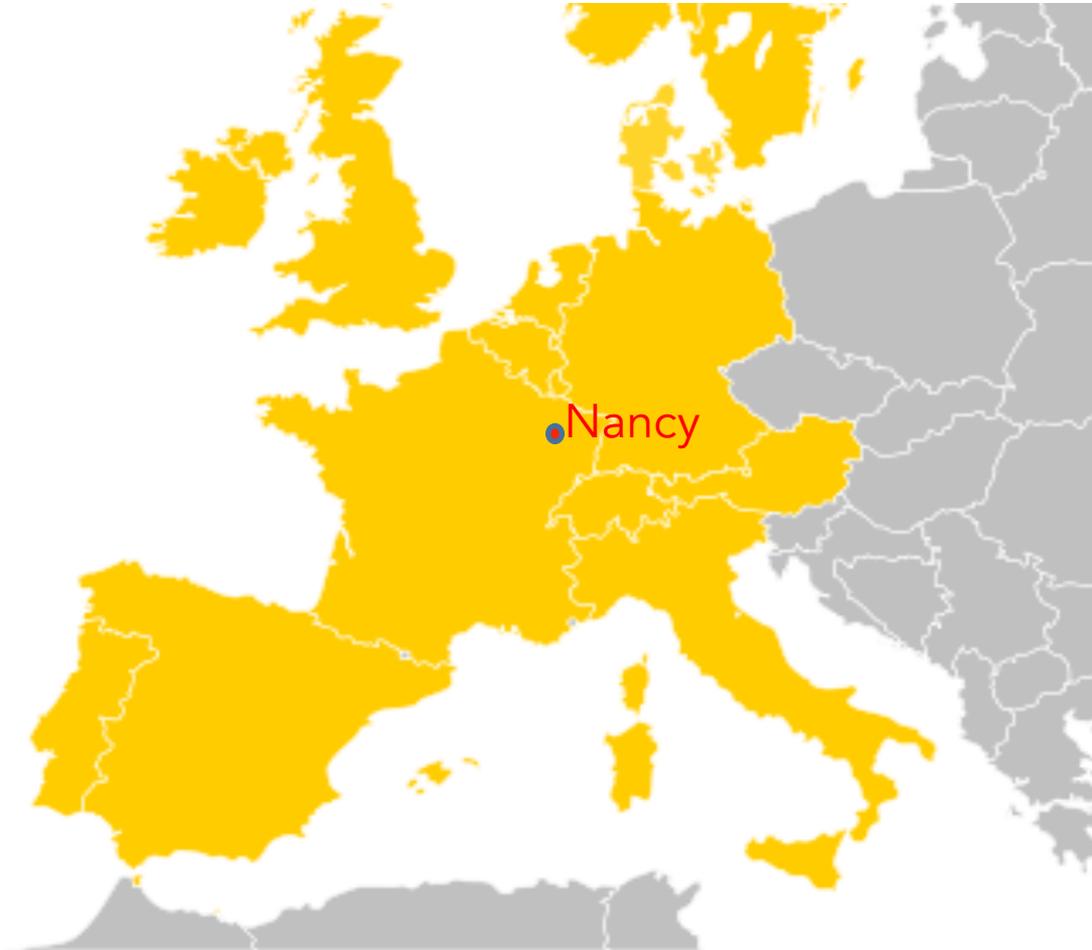
Universitat Jaume I | September 2016

Olivier POTIER

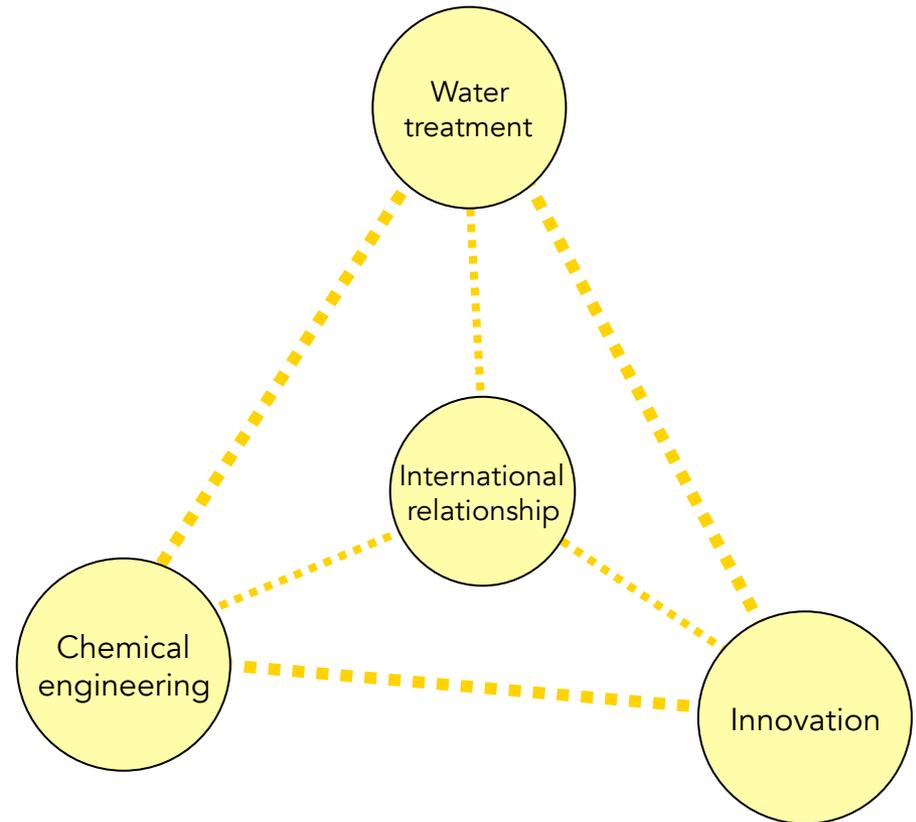
Laboratoire Réactions et Génie des Procédés / E.N.S.G.S.I.

C.N.R.S. / Université de Lorraine

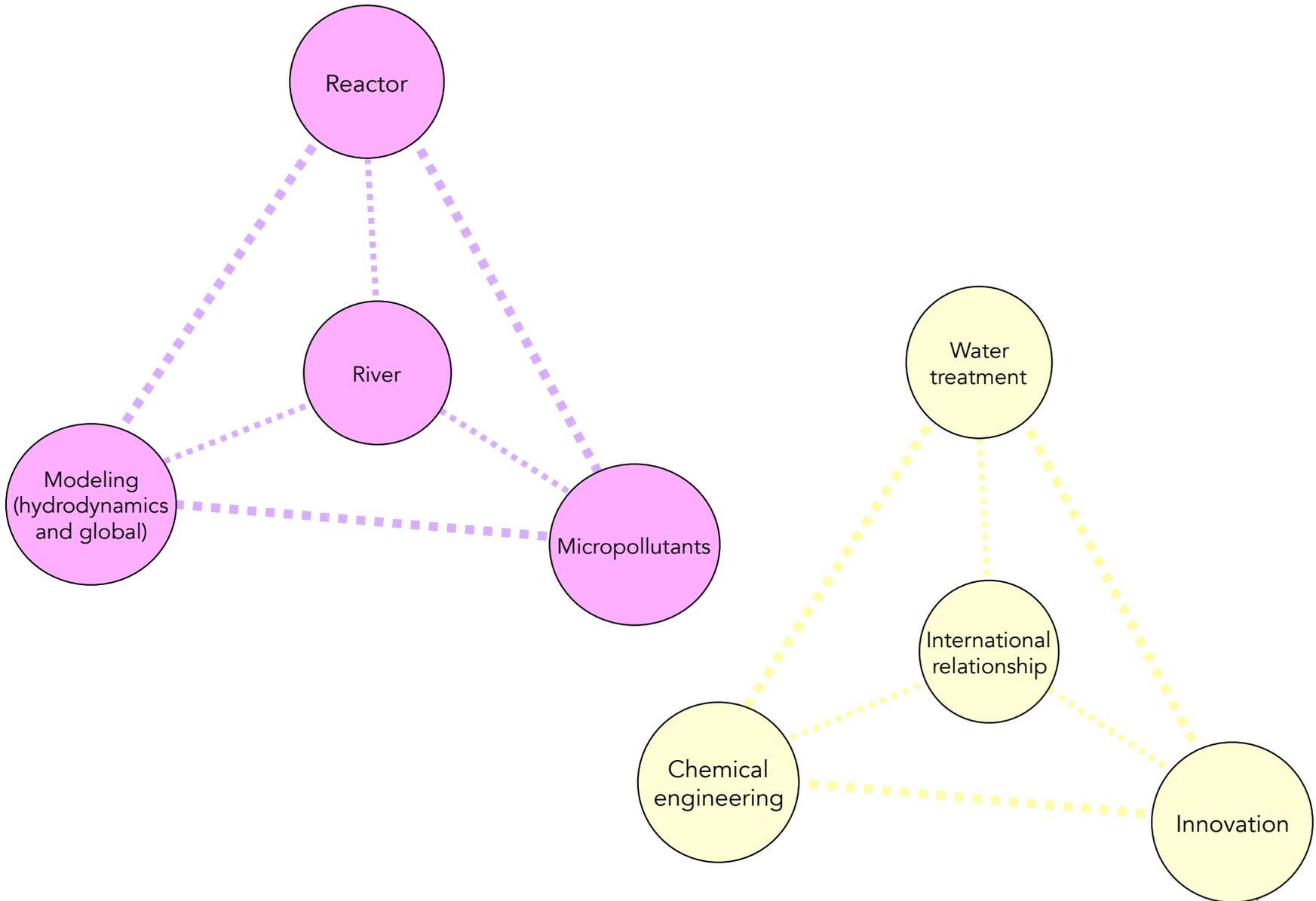
City of Nancy



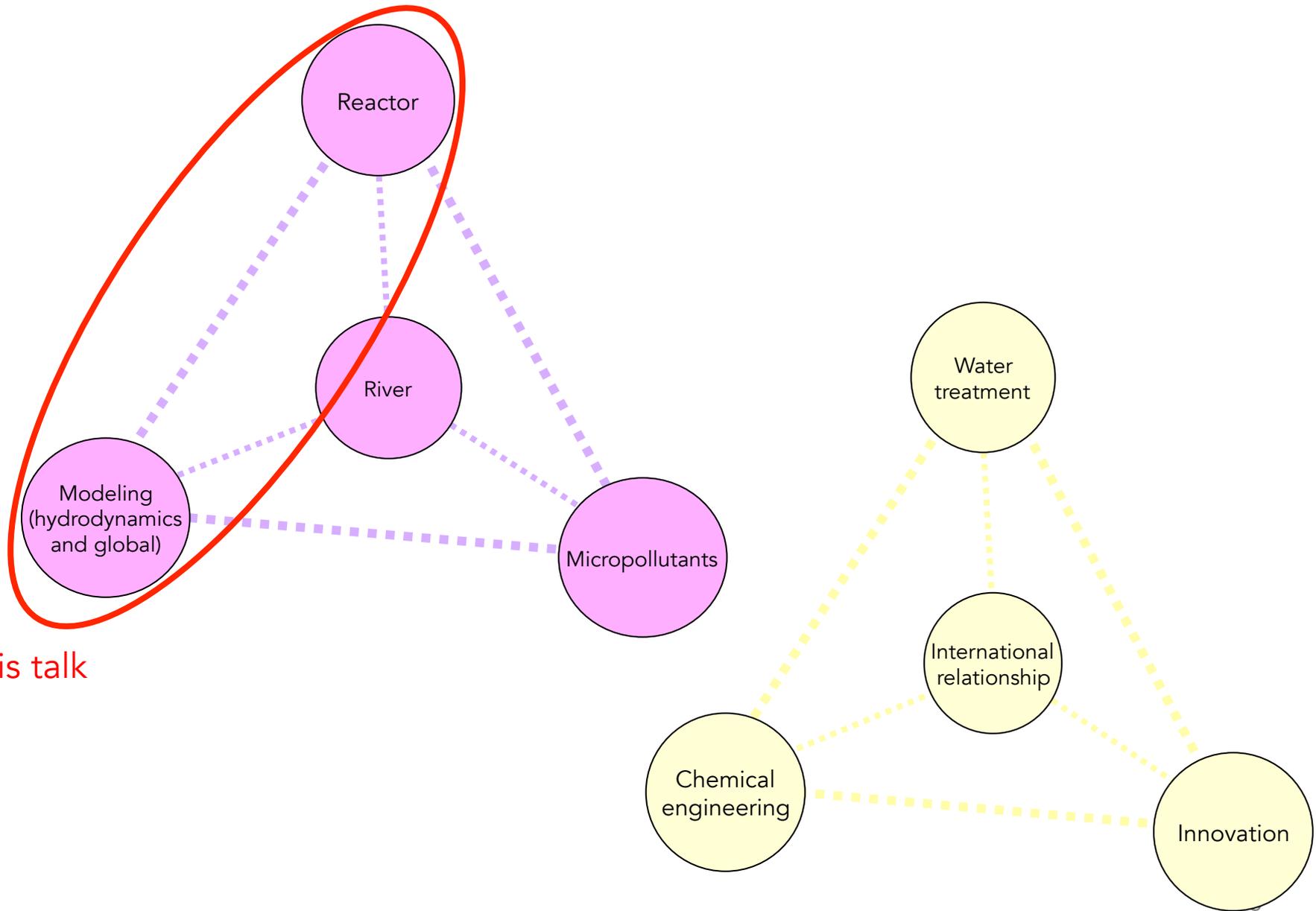
Personal interests



Personal interests



Personal interests



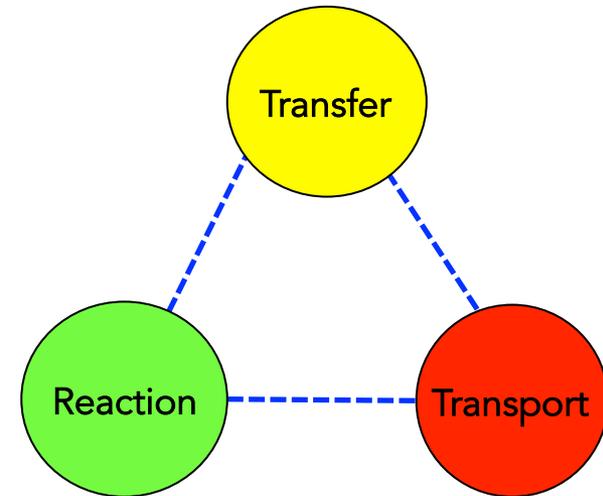
Why Modeling and Simulation?

- To simply simulate!
- To control the process.
- To try to optimize the whole processes; indeed, only to improve some parts of it.
- To forecast the released pollution.
- But also to deeply study the process and have a new tool for design.

Keywords

The 3 keywords of Chemical engineering:

Transfer
Transport
Reaction



=> Hydrodynamics is really important

Hydrodynamics

It is very important to know the space distribution of the fluid; so where the Compounds are going to react.

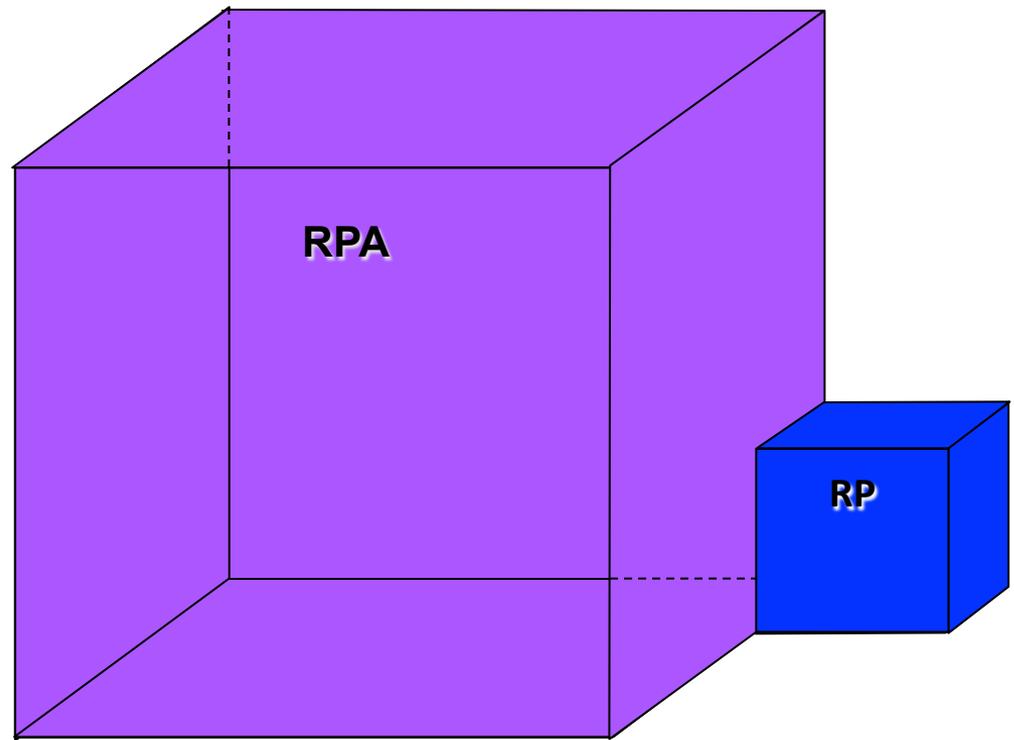
But

Hydrodynamics

Hydrodynamics is not only a space distribution of compounds, which react at different places,

but also

a useful tool for optimization of the process design by "joining" effects of reactions and transport (and transfer).



Exemple :

- On traite 10 m³/h de solution de réactif A
- Réaction chimique d'ordre 1 ($k = 4 \text{ h}^{-1}$)
- Taux de conversion souhaité : 99 %

Opération continue dans un Réacteur Parfaitement Agité :

Le volume du réacteur RPA est donc : $V_{RPA} = \tau Q = 248 \text{ m}^3$

Opération continue dans un Réacteur Piston :

Le volume du réacteur piston est donc : $V_{RP} = \tau Q = 11,5 \text{ m}^3$

Ici :

$$\frac{V_{RPA}}{V_{RP}} \approx 22$$

Hydrodynamics

Hydrodynamics is not only a space distribution of compounds, which react at different places,

but also

a useful tool for optimization of the process design by “joining” effects of reactions and transport (and transfer).

Therefore, Hydrodynamics is also a tool to improve the performance; increasing the reaction yields, reducing the reactor size and costs.

Hydrodynamics

Necessary to use an integrated approach using Reaction, Hydrodynamics and eventually Transfer;

theoretically,
experimentally,
and also with
simulations.

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Hydrodynamics

Necessary to use an integrated approach using Reaction, Hydrodynamics and eventually Transfer;

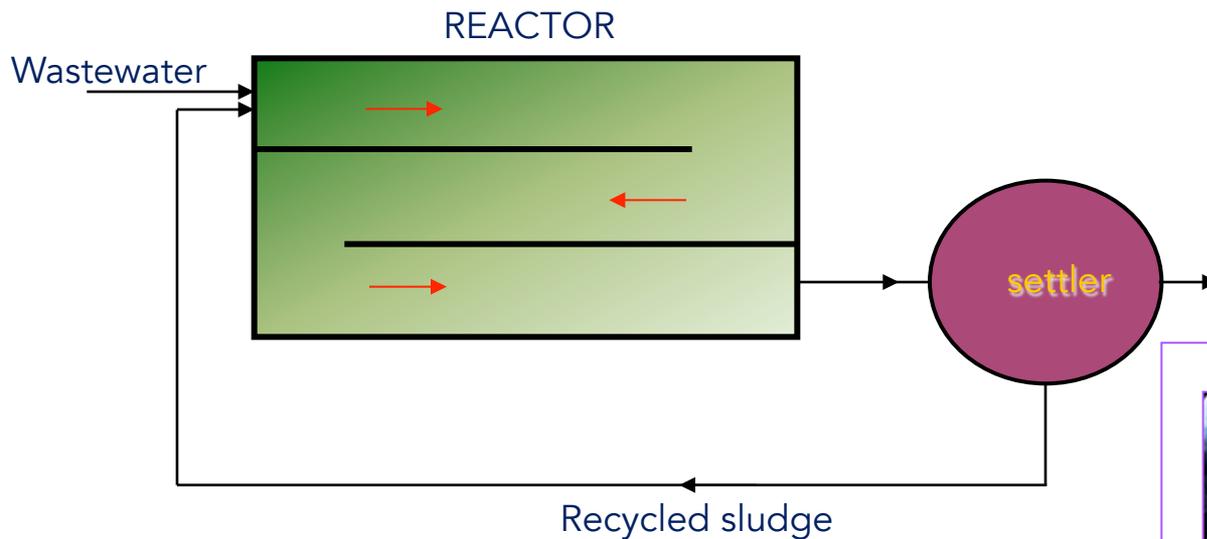
theoretically,
experimentally,
and also with
simulations.

But first,

it is necessary
to understand and model
the hydrodynamics.

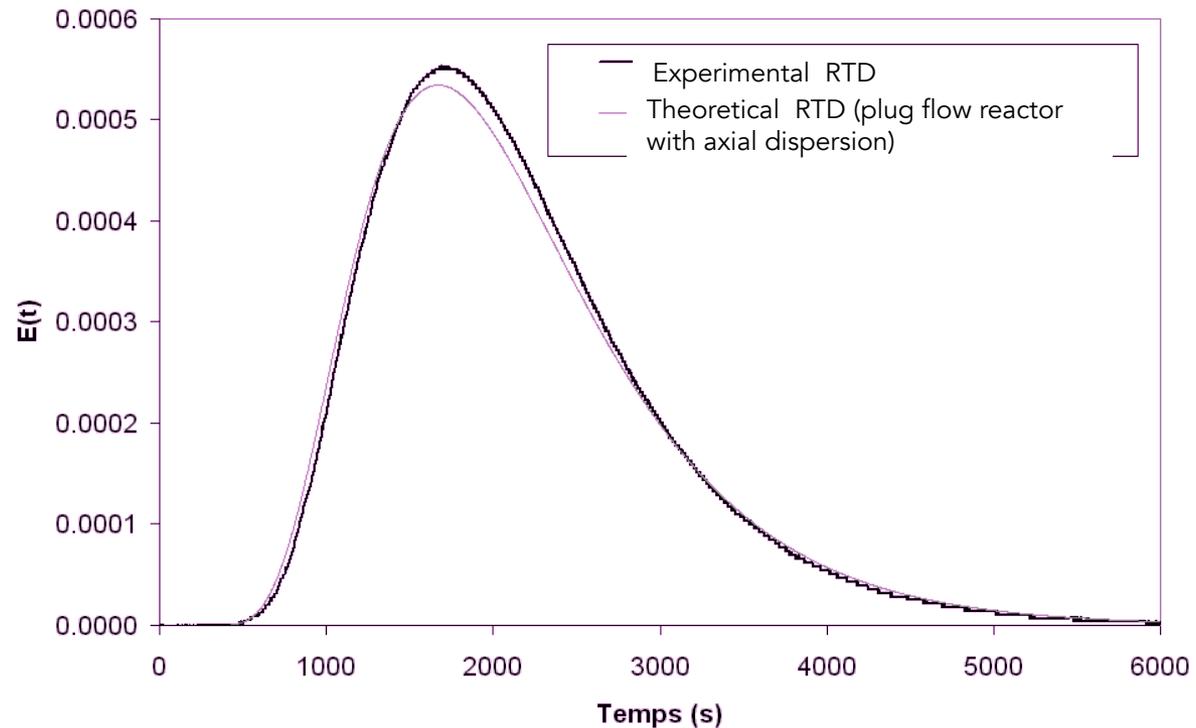
Therefore, Hydrodynamics is also a tool to improve the performance; increasing the reaction yields, reducing the reactor size and costs.

Wastewater treatment reactors



Example of the channel reactor:
volume 3300 m^3 , total length 102 m, width 9 m,
depth 3.6 m

Tracing in the full-scale plant of Nancy: residence time distributions



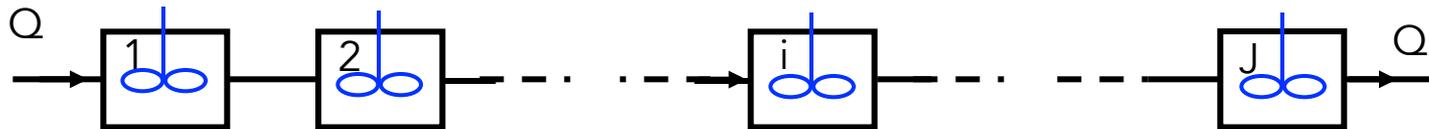
Hydrodynamic model : Series of CSTR or Plug flow reactor with axial dispersion

Hydrodynamic model

Plug flow reactor with axial dispersion
Characterized by the Peclet number (Pe)

$$Pe = \frac{u.L}{D}$$

Series of CSTR
Characterized by J



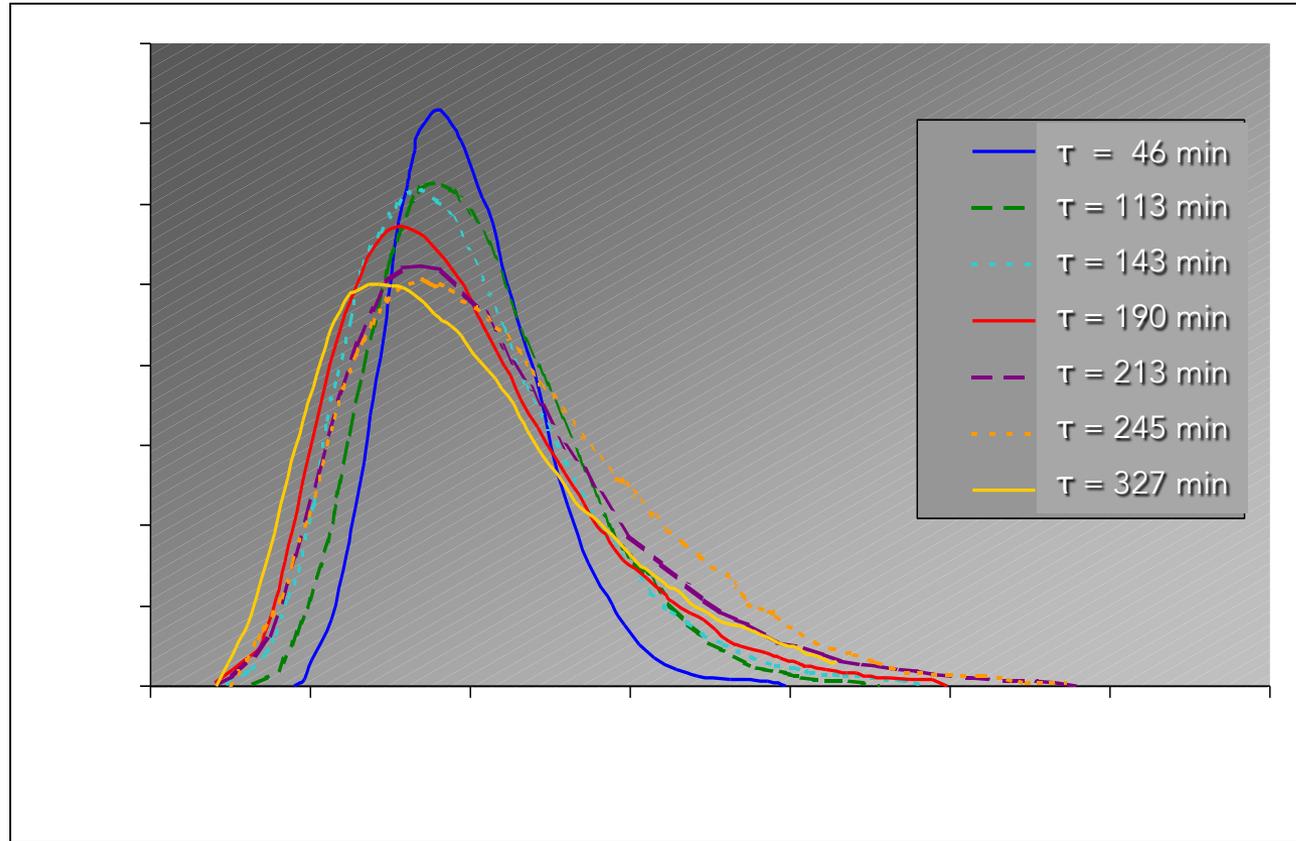
Wastewater treatment reactors

Modeling the hydrodynamic variation
(effect of flowrate)

Forecasting the reactor hydrodynamic without having
expensive tracer experiments

Residence Time Distributions for different space-times (τ) in a channel reactor pilot plant

With same geometry (same width w , same height H) and same gas flowrate



Comparison between theoretical curve and experimental data

Plug flow reactor with axial dispersion

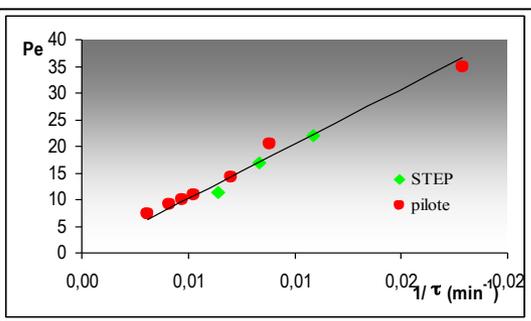
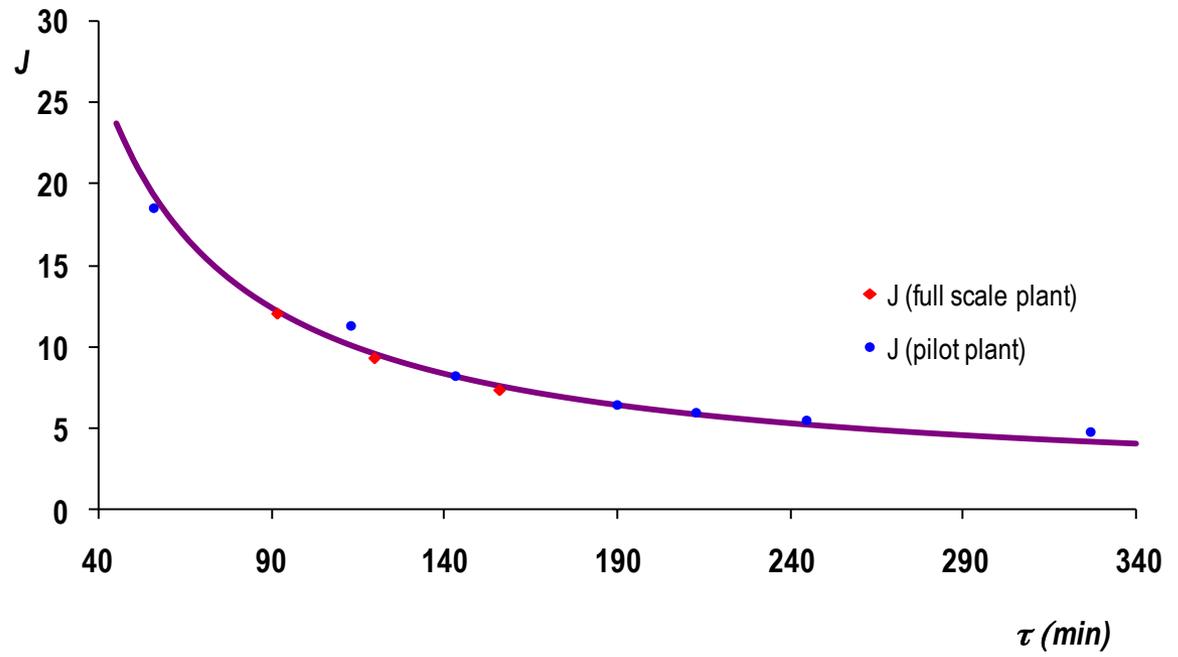
$$P = \frac{u.L}{D} = \frac{L^2}{D.\tau}$$

Series of CSTR

$$J \cong \frac{L^2}{2D\tau} + 1$$

$$J \cong 1 + \frac{K}{\tau}$$

$$\text{with } K = \frac{L^2}{2D}$$



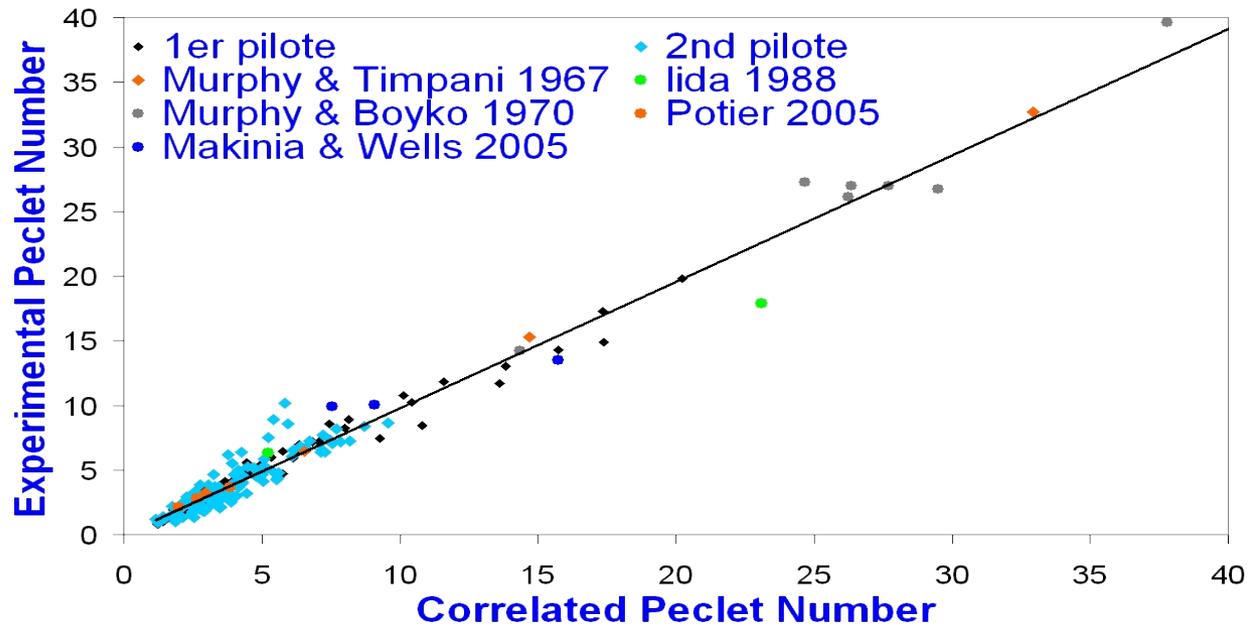
Reactor hydrodynamic modeling

- 3 pilot plants
 - 1 WWTP (Nancy)
 - 194 data from the literature
- } Correlation
P = f (adimensional numbers)

Modeling using the Buckingham π Theorem

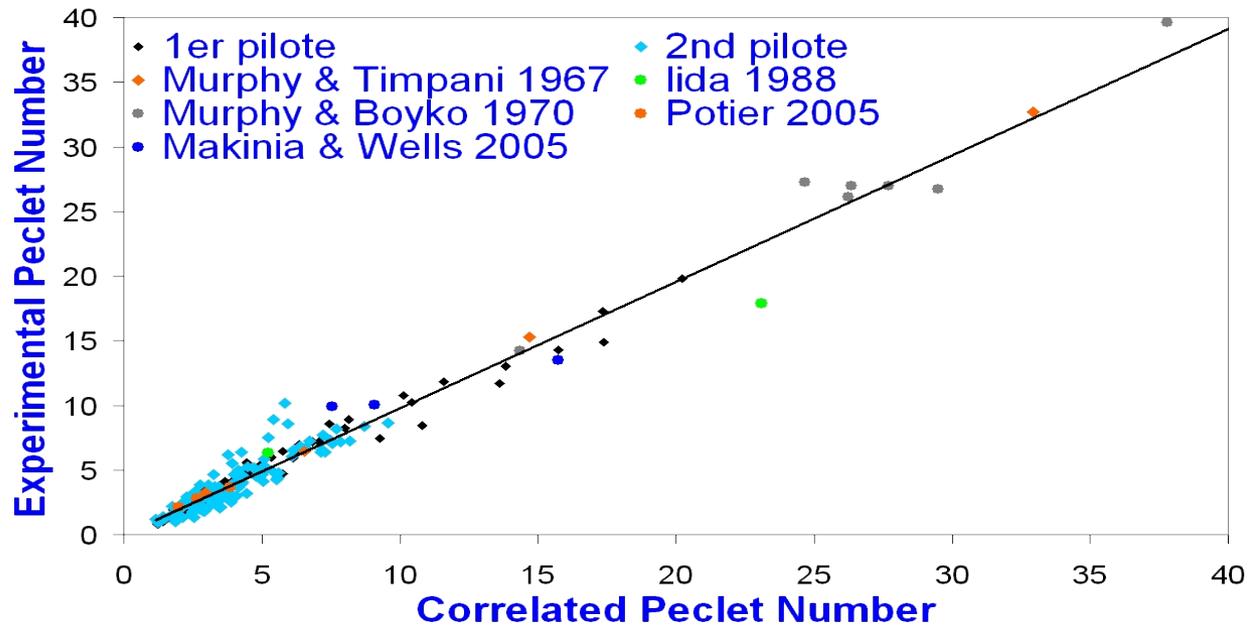
$$Pe = 0,0264 \left(\frac{\mu_L \cdot DH_h}{Q_L \rho_L} \right)^{-0,102} \left(\frac{DH_h}{DH_v} \right)^{-0,908} \left(\frac{g \cdot DH_h^5}{Q_L^2} \right)^{0,309} \left(\frac{Q_G}{Q_L} \right)^{0,468} \left(\frac{l_{a\acute{e}ration}}{l} \right)^{0,438}$$

Reactor hydrodynamic modeling



$$Pe = 0,0264 \left(\frac{\mu_L \cdot DH_h}{Q_L \rho_L} \right)^{-0,102} \left(\frac{DH_h}{DH_v} \right)^{-0,908} \left(\frac{g \cdot DH_h^5}{Q_L^2} \right)^{0,309} \left(\frac{Q_G}{Q_L} \right)^{0,468} \left(\frac{l_{a\acute{e}ration}}{l} \right)^{0,438}$$

Reactor hydrodynamic modeling



$$D = \frac{2}{3} \frac{h}{h+w} \sqrt{\frac{Q_G \cdot w_{aeration} (L+w)}{2}}$$

Wastewater Treatment: Approach to Modeling Transport, Transfer and Reactions

Wastewater Treatment: Approach to Modeling Transport, Transfer and Reactions

Reactor

Systemic approach

CFD with reaction

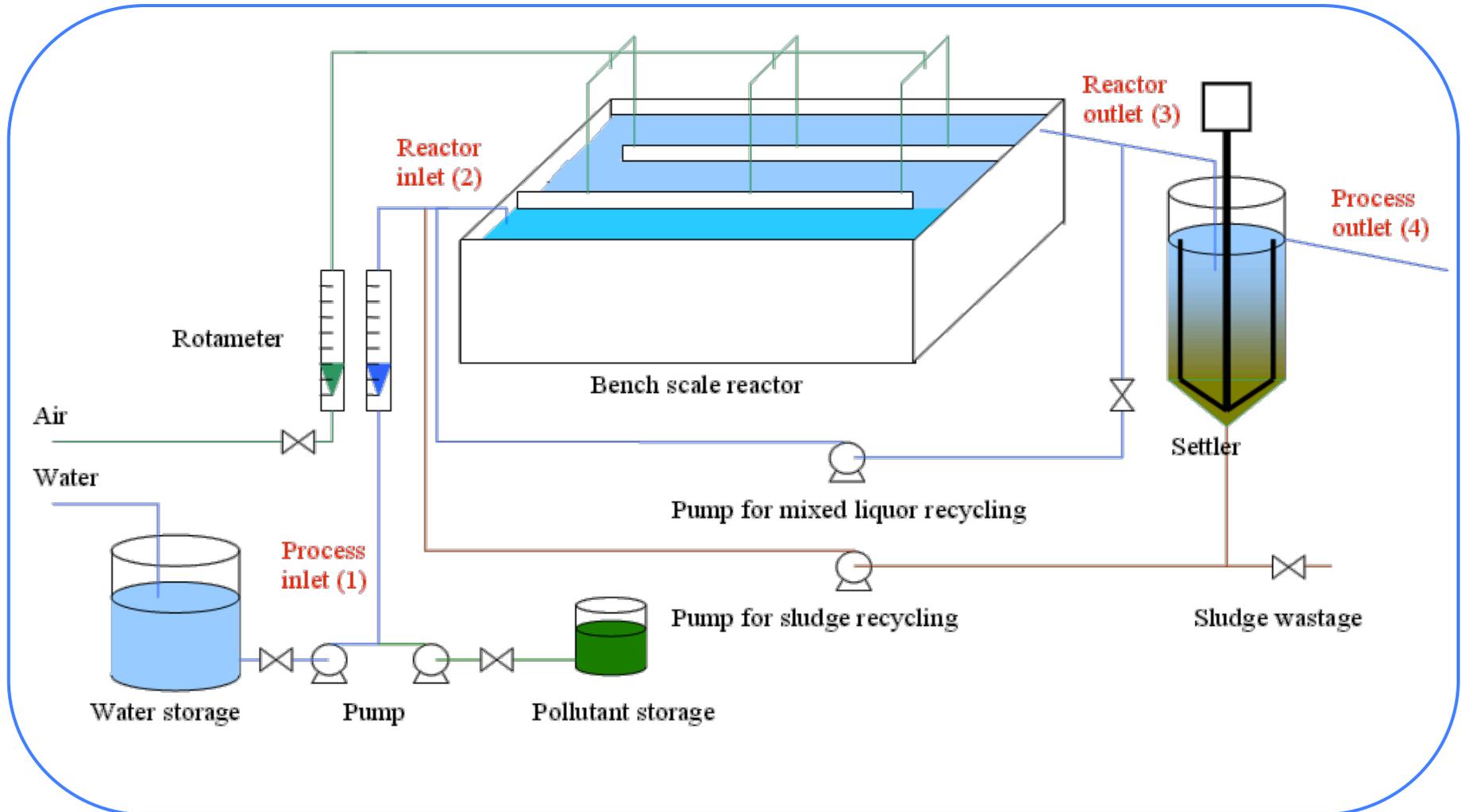
Compartmental methodology

Objectives

Modeling and Simulate Transport, Transfer, and Reactions comparing 3 approaches:

- **Systemic model obtained by tracing**
Generally 5 to 20 elementary cells (CSTR)
- **Computational Fluid Dynamics (CFD) with reactions**
High number of cells
- **New approach: compartmental modeling**
New discretization method: 10 to 2000 cells

Reactor and biological reaction



Kinetics modeling ASM1

S_I : Soluble inert organic matter

S_S : Readily biodegradable substrate

X_I : Particulate inert organic matter

X_S : Slowly biodegradable substrate

$X_{B,H}$: Active heterotrophic biomass

$X_{B,A}$: Active autotrophic biomass

X_P : Particulate products arising from biomass decay

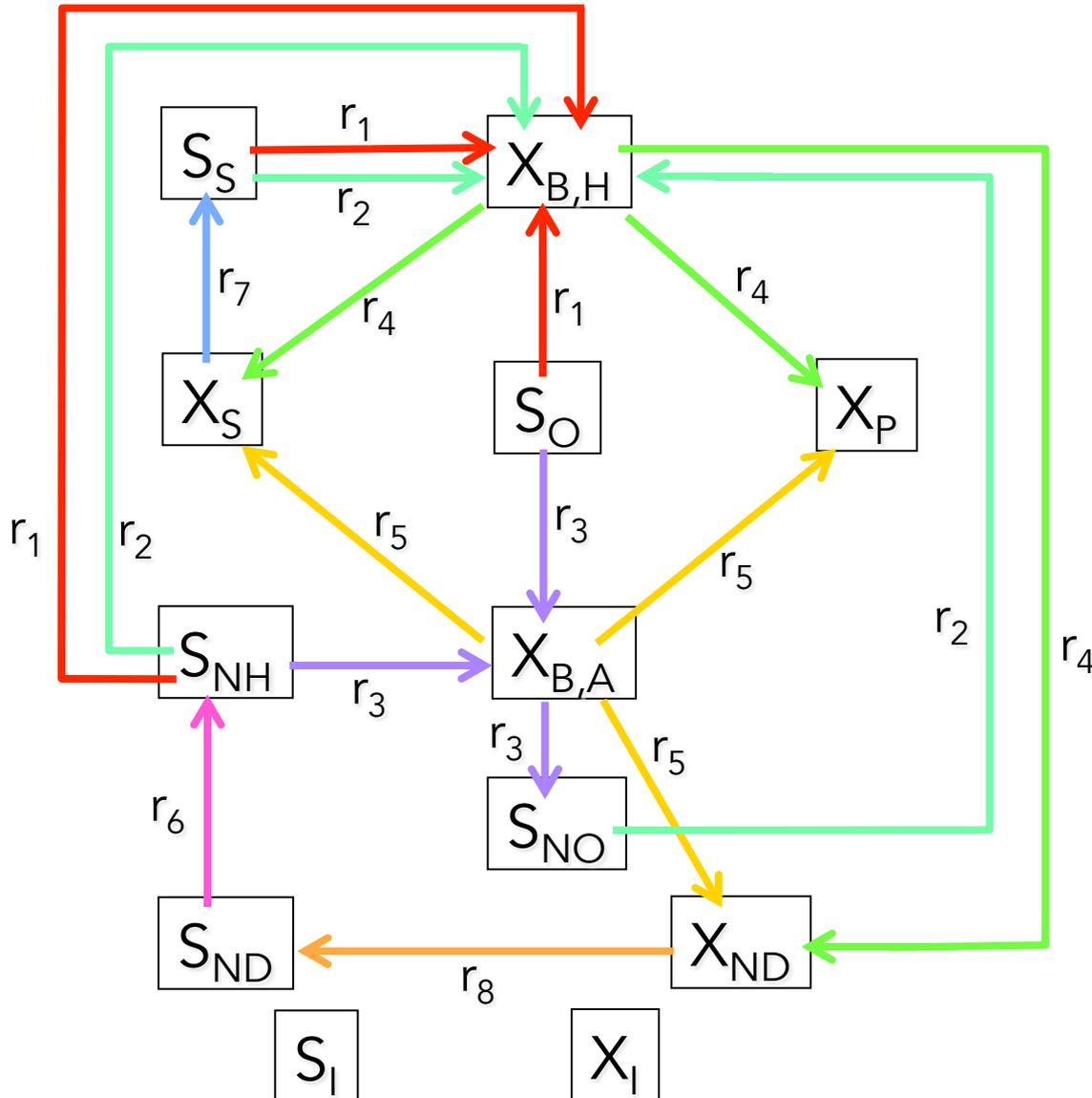
S_O : Oxygen

S_{NO} : Nitrate and nitrite nitrogen

S_{NH} : NH_4^+ and NH_3 nitrogen

S_{ND} : Soluble biodegradable organic nitrogen

X_{ND} : Particulate biodegradable organic nitrogen



Kinetics modeling ASM1

Anoxic growth of heterotrophs

$$\rho_2 = \mu_H \left(\frac{S_S}{K_S + S_S} \right) \left(\frac{K_{O,H}}{K_{O,H} + S_O} \right) \left(\frac{S_{NO}}{K_{NO} + S_{NO}} \right) \eta_g X_{B,H}$$

Aerobic growth of heterotrophs

$$\rho_1 = \mu_H \left(\frac{S_S}{K_S + S_S} \right) \left(\frac{S_O}{K_{O,H} + S_O} \right) X_{B,H}$$

Aerobic growth of autotrophs

$$\rho_3 = \mu_A \left(\frac{S_{NH}}{K_{NH} + S_{NH}} \right) \left(\frac{S_O}{K_{O,A} + S_O} \right) X_{B,A}$$

Decay of heterotrophs

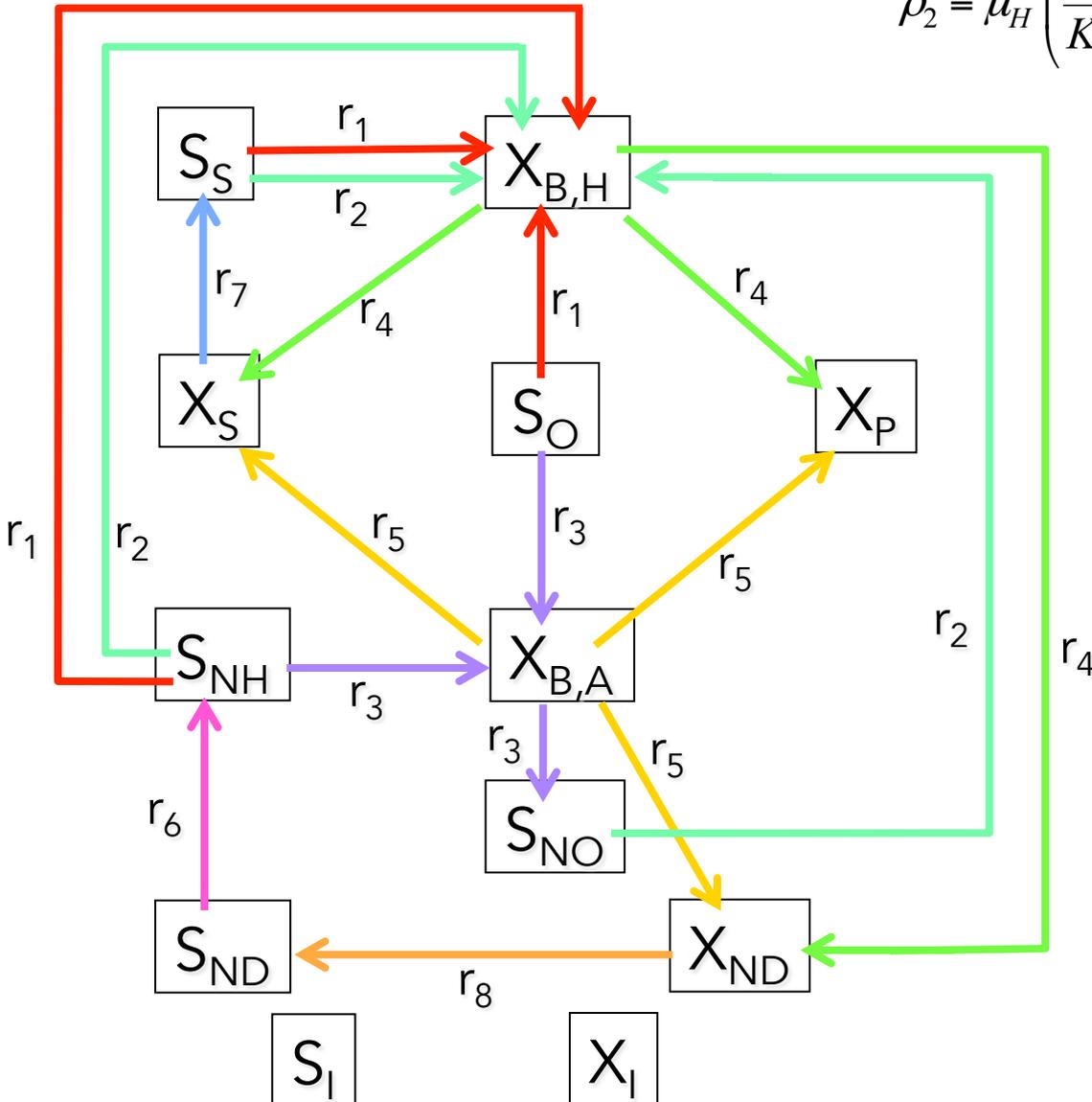
$$\rho_4 = b_H X_{B,H}$$

Decay of autotrophs

$$\rho_5 = b_A X_{B,A}$$

Ammonification of soluble organic nitrogen

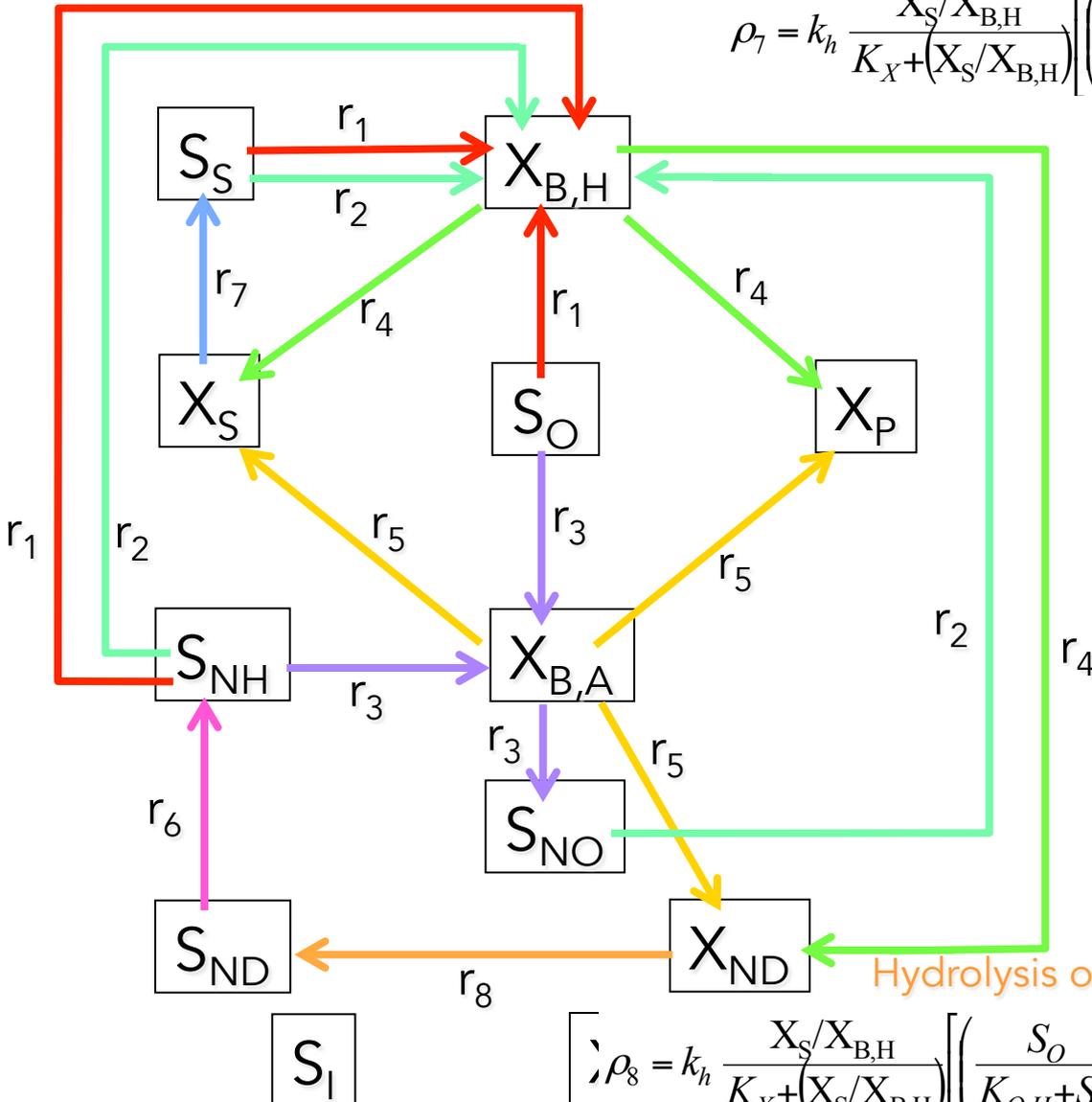
$$\rho_6 = k_a S_{ND} X_{B,H}$$



Kinetics modeling ASM1

Hydrolysis of entrapped organics

$$\rho_7 = k_h \frac{X_S/X_{B,H}}{K_X + (X_S/X_{B,H})} \left[\left(\frac{S_O}{K_{O,H} + S_O} \right) + \eta_h \left(\frac{K_{O,H}}{K_{O,H} + S_O} \right) \left(\frac{S_{NO}}{K_{NO} + S_{NO}} \right) \right] X_{B,H}$$



Hydrolysis of entrapped organic nitrogen

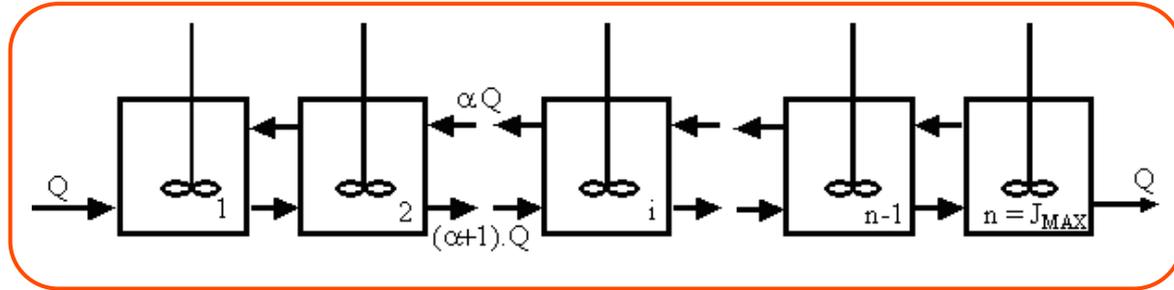
$$\rho_8 = k_h \frac{X_S/X_{B,H}}{K_X + (X_S/X_{B,H})} \left[\left(\frac{S_O}{K_{O,H} + S_O} \right) + \eta_h \left(\frac{K_{O,H}}{K_{O,H} + S_O} \right) \left(\frac{S_{NO}}{K_{NO} + S_{NO}} \right) \right] X_{B,H} (X_{ND}/X_S)$$

Simulation with reactions

systemic approach

Systemic modeling

CSTR in series with backmixing, enabling to take into account the hydrodynamics changes



$$G(s) = (1 + \alpha) \left[\frac{1 + \alpha}{\alpha} \right]^{J_{\max} - 1} \left\{ \frac{2\sqrt{\gamma^2 - 4\alpha(1 + \alpha)}}{2\alpha B} \right\} \quad (16)$$

with

$$B = \left(\frac{1 + \alpha}{\alpha} \right) \left\{ \left(\frac{\gamma - \sqrt{\gamma^2 - 4\alpha(1 + \alpha)}}{2\alpha} \right)^{J_{\max} - 2} Y_- - \left(\frac{\gamma + \sqrt{\gamma^2 - 4\alpha(1 + \alpha)}}{2\alpha} \right)^{J_{\max} - 2} Y_+ \right\} \quad (17)$$

and

$$\gamma = 1 + 2\alpha + \frac{\tau \cdot s}{J_{\max}}, \quad (18)$$

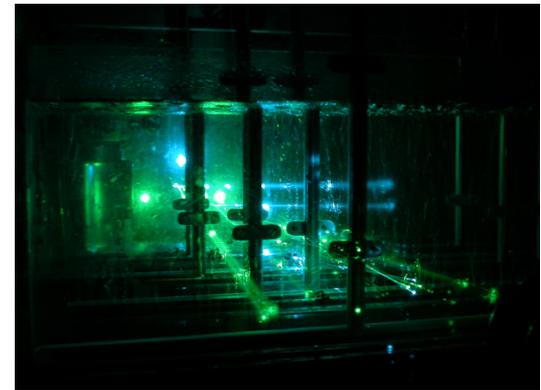
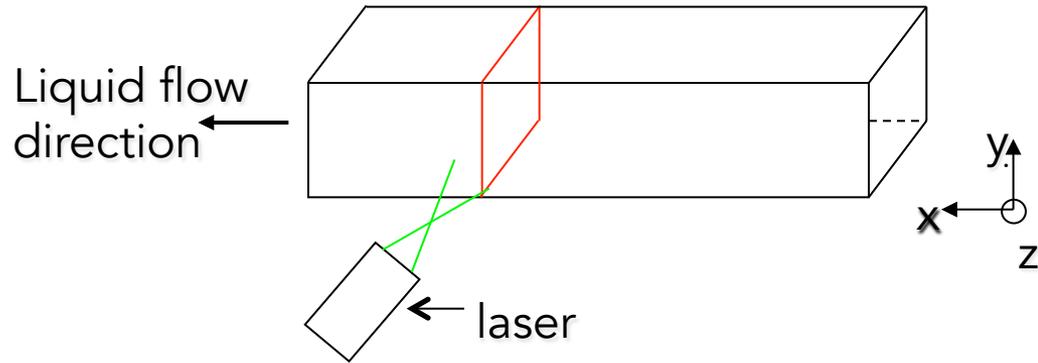
$$Y_- = \left[1 + \alpha + \frac{\tau \cdot s}{J_{\max}} - \alpha \frac{\gamma + \sqrt{\gamma^2 - 4\alpha(1 + \alpha)}}{2\alpha} \right] \left[(1 + \alpha) - \left(1 + \alpha + \frac{\tau \cdot s}{J_{\max}} \right) \frac{\gamma - \sqrt{\gamma^2 - 4\alpha(1 + \alpha)}}{2\alpha} \right],$$

$$Y_+ = \left[1 + \alpha + \frac{\tau \cdot s}{J_{\max}} - \alpha \frac{\gamma - \sqrt{\gamma^2 - 4\alpha(1 + \alpha)}}{2\alpha} \right] \left[(1 + \alpha) - \left(1 + \alpha + \frac{\tau \cdot s}{J_{\max}} \right) \frac{\gamma + \sqrt{\gamma^2 - 4\alpha(1 + \alpha)}}{2\alpha} \right]$$

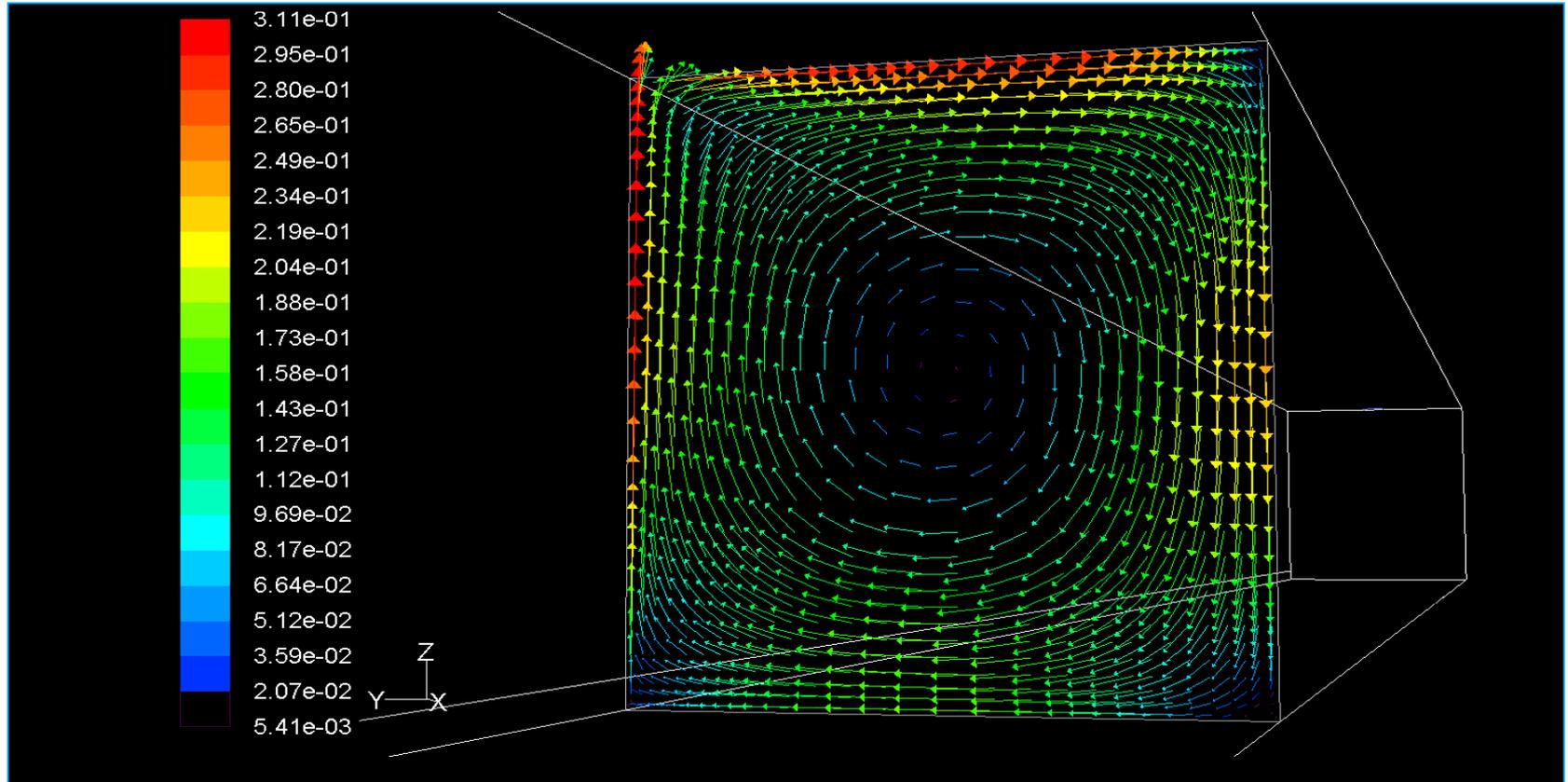
$$\alpha = \frac{1}{2} \left[(J_{\max} - 1) - \left(1 + J_{\max}^2 \left(1 - \frac{2}{J_{\text{app}}} \right) \right)^{1/2} \right]$$

LDA and CFD Simulation with reactions

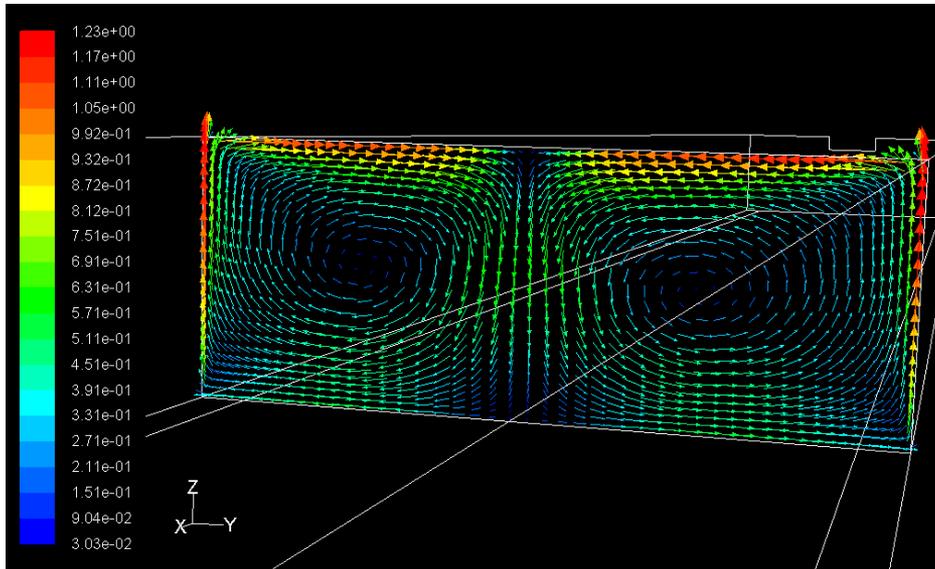
Laser Doppler Anemometry



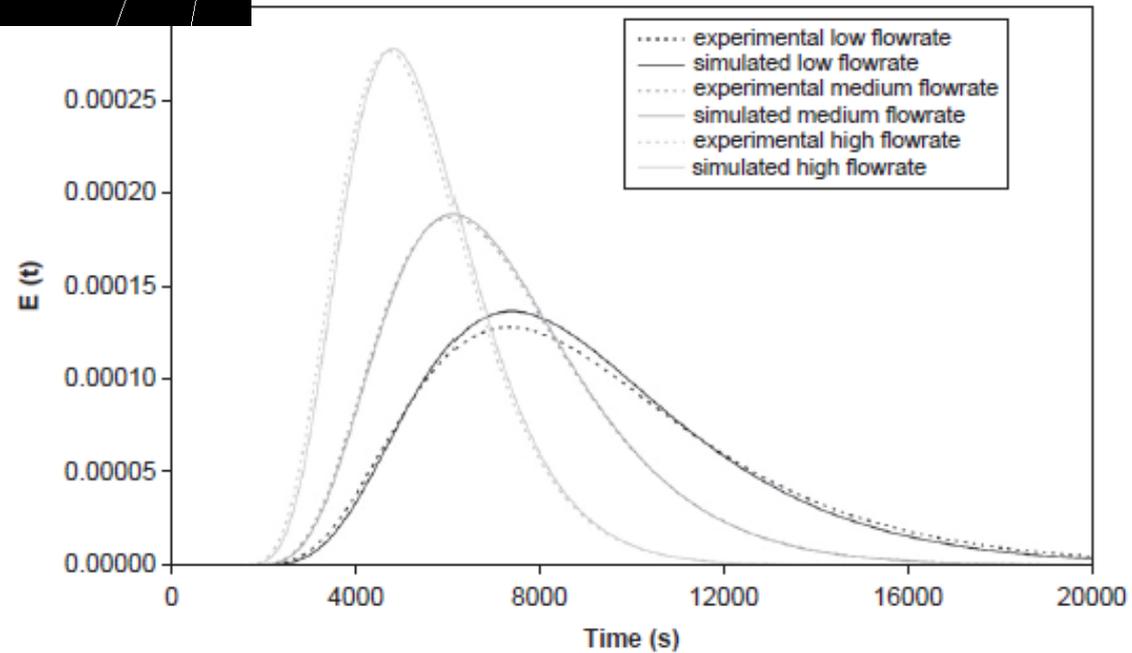
CFD modeling



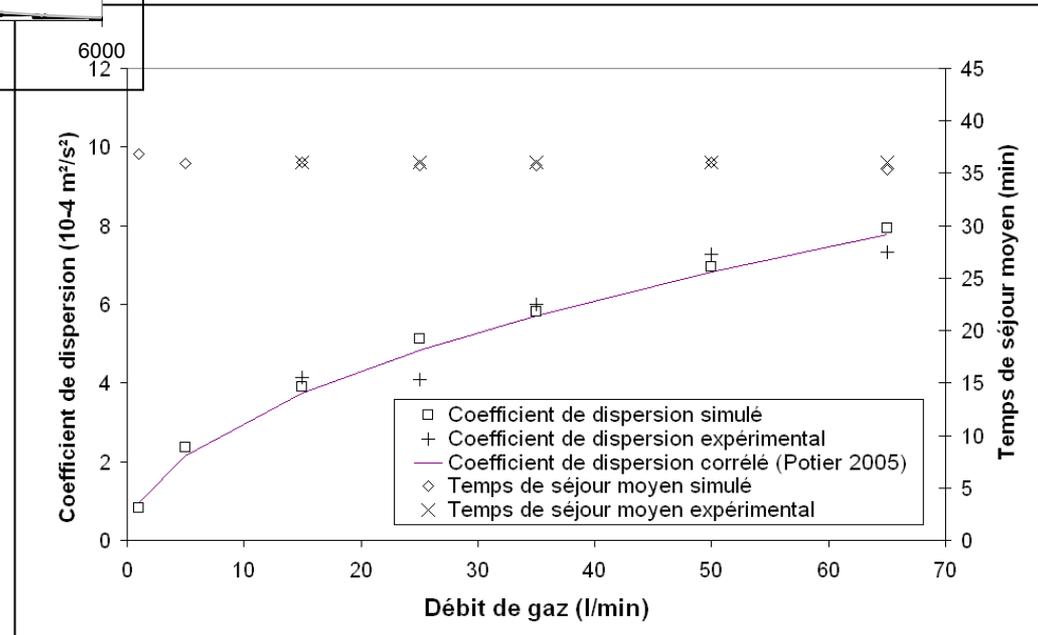
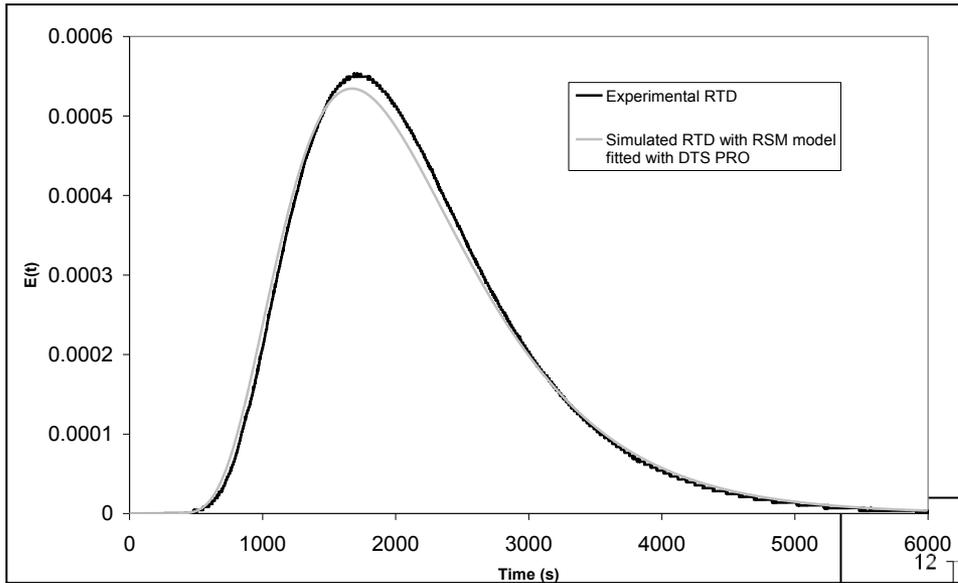
CFD modeling



WWTP Nancy-Maxéville



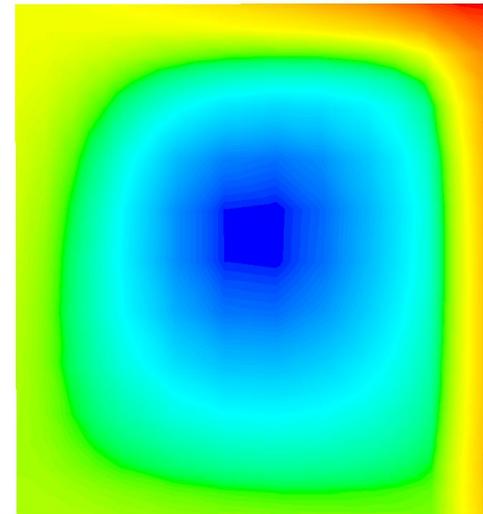
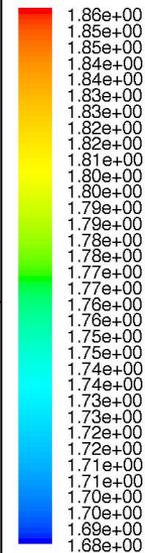
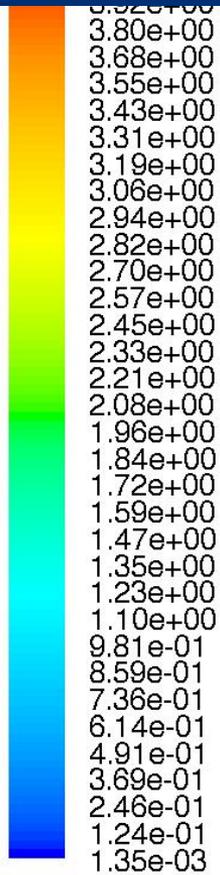
CFD modeling – Residence Time Distribution



CFD with Reactions

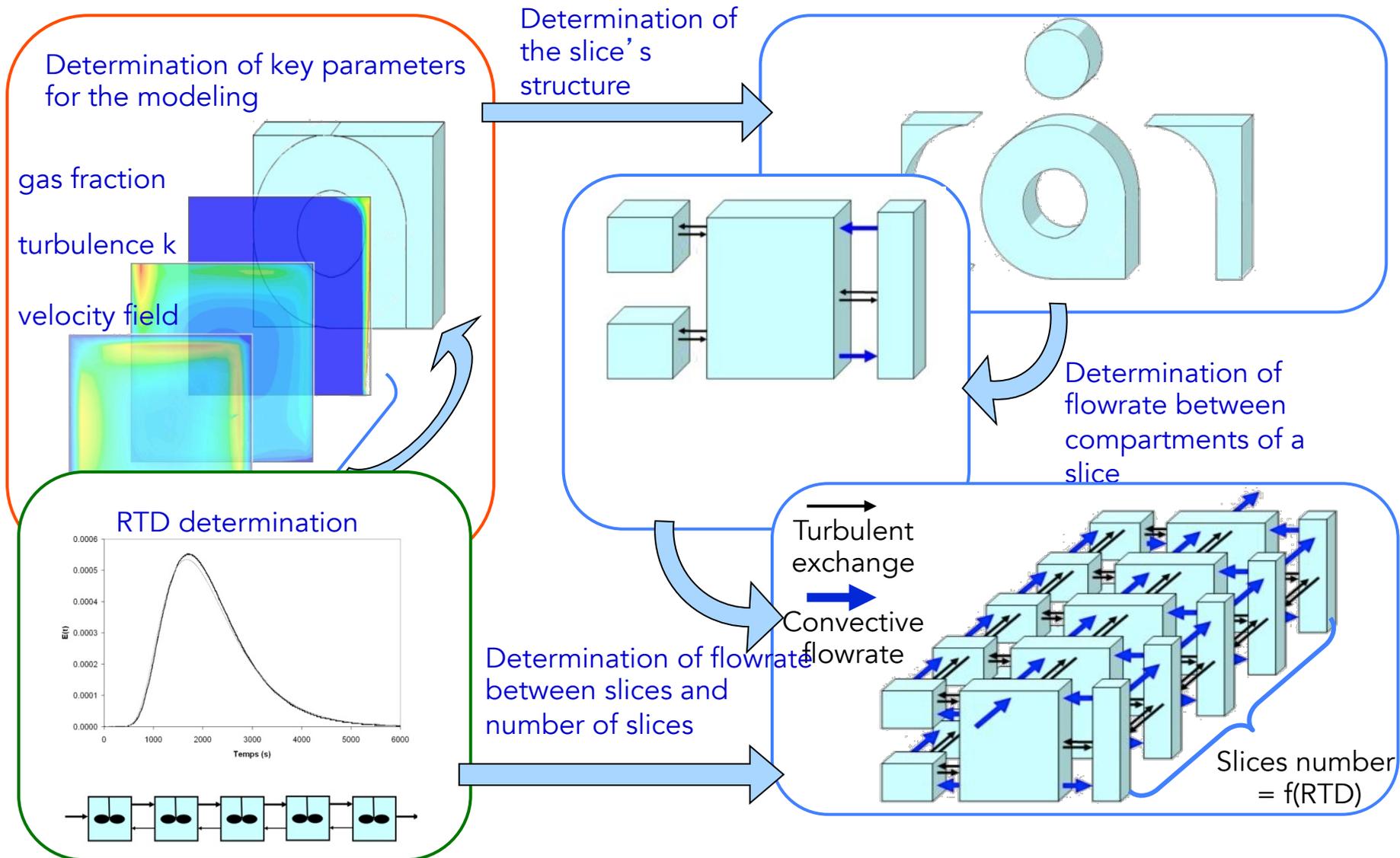
CFD with reactions

Dissolved oxygen



Compartmental modeling

Compartmental approach



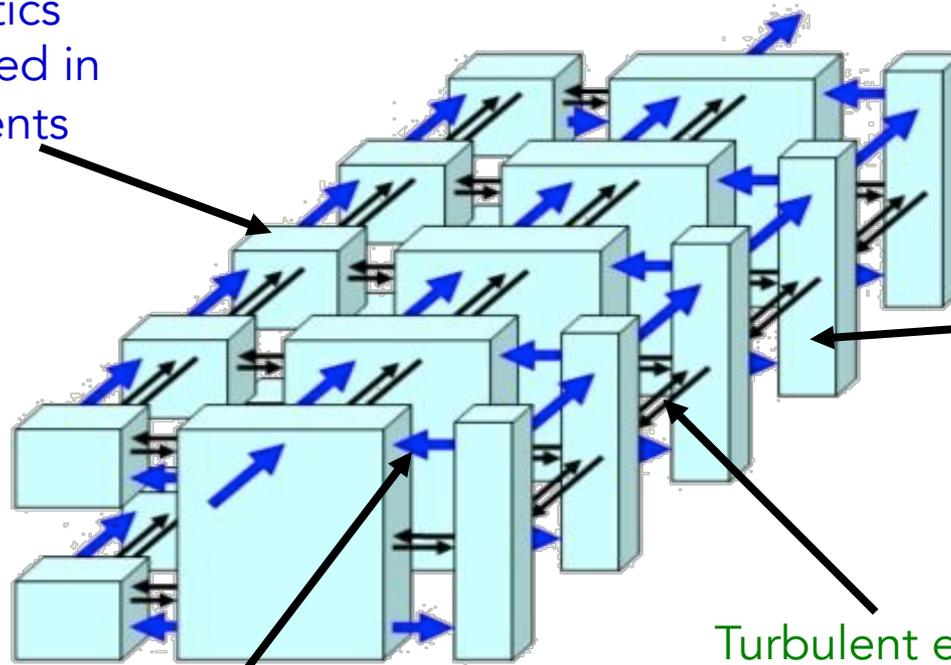
Compartmental approach: summary

ASM1 kinetics model added in compartments

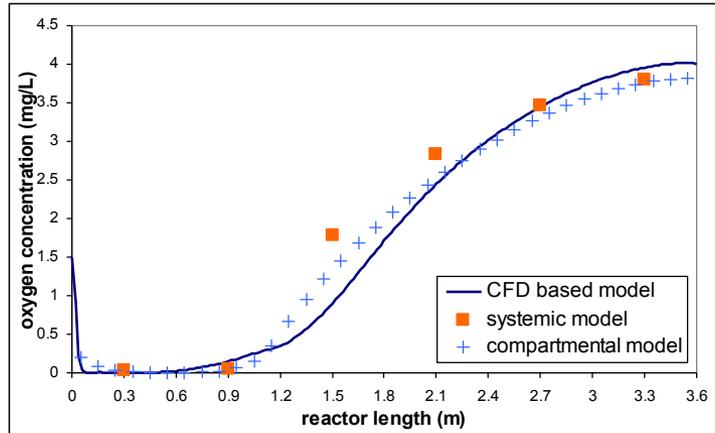
Gas-liquid transfer added in rich-gas compartments

Convective flowrate calculated from CFD mean velocity fields

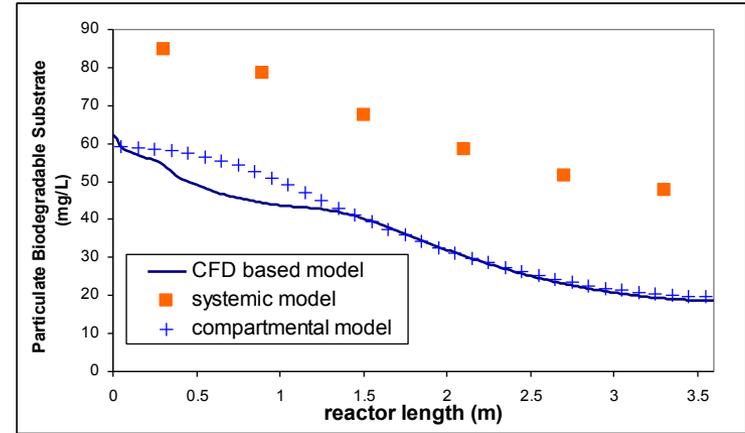
Turbulent exchange flowrates and number of slices calculated from simulated turbulence and RTD (by an iterative procedure)



Comparison of models

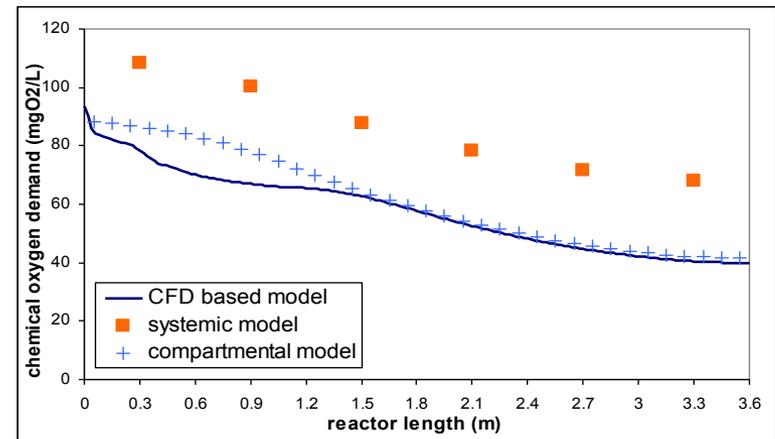


Three models give almost the same results for dissolved oxygen concentration



For X_S (slowly biodegradable substrate)

$$DCO = S_1 + S_S + X_1 + X_S$$



- The three models follow the same trend
- CFD and compartment model look very similar

Compartmental modeling; another approach

Towards better models for describing mixing using compartmental modelling: a full-scale case demonstration

Usman Rehman¹, Chaim De Mulder¹, Youri Amerlinck¹, Marina Arnaldos², Stefan R. Weijers³, Olivier Potier⁴, and Ingmar Nopens¹

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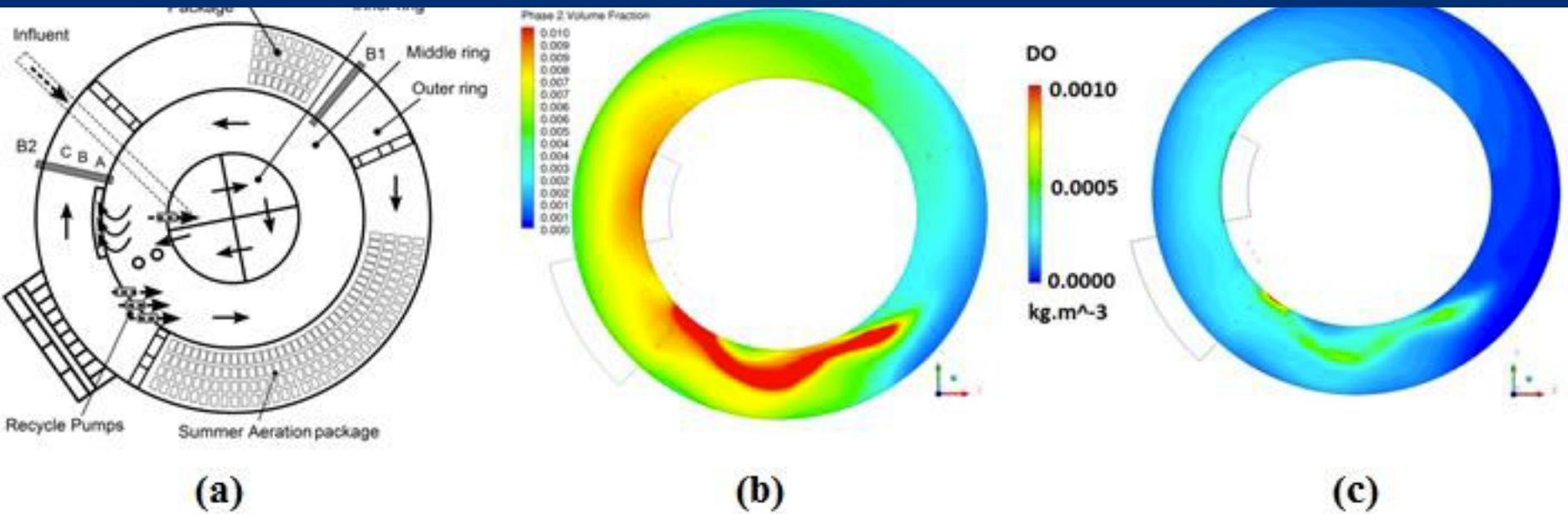
3 Waterschap De Dommel, Bosscheweg 56, 5283 WB Boxtel, Postbus 10.001, Netherlands

4 Laboratoire Réactions et Génie des Procédés, LRGP, CNRS UMR 7274, Université de Lorraine, 1 rue Grandville, BP 20451, 54001 NANCY cedex, France



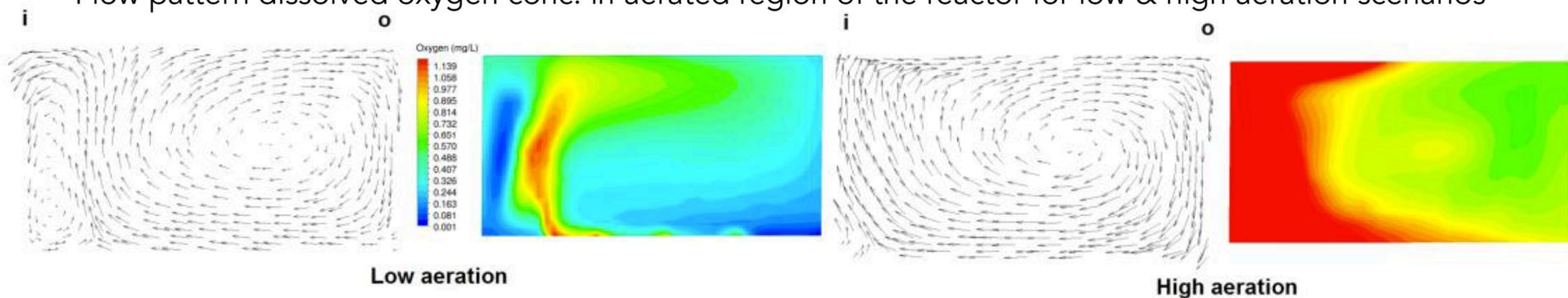
Compartmental modeling; another approach.

Usman Rehman's PhD



(a) Reactor configuration (b) Gas fraction distribution in the reactor (c) Dissolved oxygen concentration in the reactor

Flow pattern dissolved oxygen conc. in aerated region of the reactor for low & high aeration scenarios



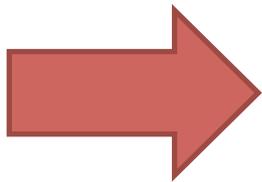
Working Group on
Computational Fluid Dynamics (CFD) & Wastewater

WG Members

- WG composed of :
 - Consultants
 - Academics
 - People from Europe, Northern and Latin America, Australia
- Chair : Julien Laurent (University of Strasbourg, France)
- Vice-Chair : Jim Wicks (The Fluid Group, UK; vice-chair)
- Secretary : Randal Samstag (Independent Consultant, USA; secretary)
- Damien Batstone (AWMC, Australia)
- Joel Ducoste (NC State, USA)
- Alonso Griborio (Hazen & Sawyer, USA)
- Genevieve Kenny (R.V. Anderson Associates, Canada)
- Ingmar Nopens (Ghent University, Belgium; past-chair)
- Anna Karpinska Portela (University of Birmingham, England)
- Olivier Potier (LRGP, CNRS - Université de Lorraine, France)
- Nicolas Ratkovich (University of Los Andes, Columbia)
- Stephen Saunders (Ibis Group, USA)
- Ed Wicklein (Carollo Engineers, USA)

WG motivations & objectives

- No guidelines regarding GMP
- Lack of CFD training & education within environmental sector

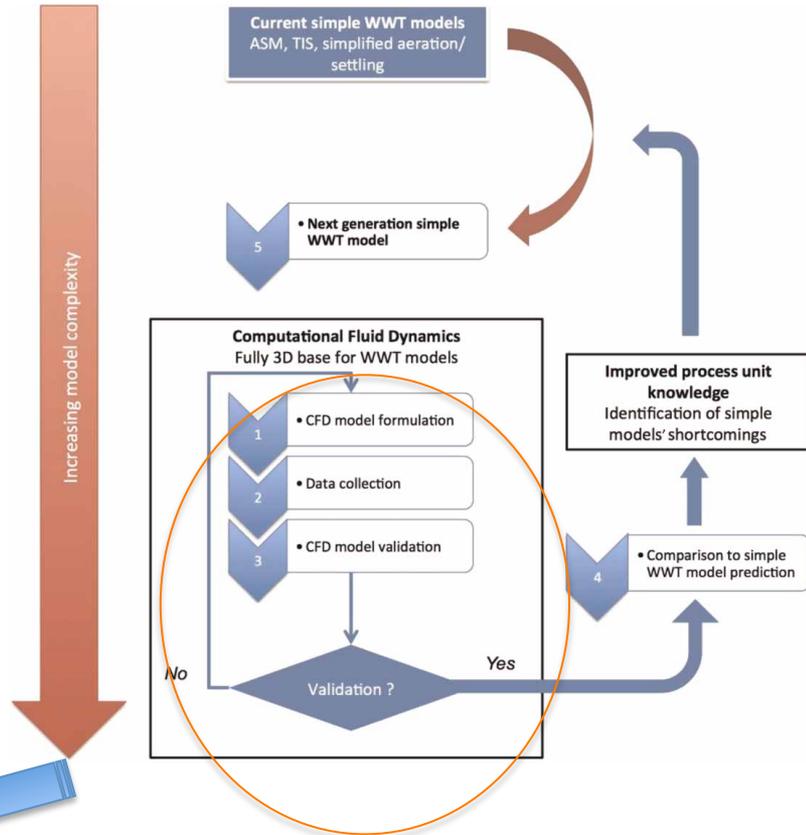


- promote the exchange of ideas and experiences regarding the use of CFD in the field of water and wastewater treatment
- build a network of experts in the field

Use of CFD in WRRF

- Troubleshooting (e.g. clarifiers)
- Hydraulics – Flow splitting
- Design improvement (clarifiers, reactors ?)
- Next generation models development

GMP required



Good modelling practice in applying computational fluid dynamics for WWTP modelling

Edward Wicklein, Damien J. Batstone, Joel Ducoste, Julien Laurent, Alonso Griborio, Jim Wicks, Stephen Saunders, Randal Samstag, Olivier Potier and Ingmar Nopens
Water Science and Technology 73 (5), 969-982

A protocol for the use of computational fluid dynamics as a supportive tool for wastewater treatment plant modelling

J. Laurent, R. W. Samstag, J. M. Ducoste, A. Griborio, I. Nopens,
D. J. Batstone, J. D. Wicks, S. Saunders and O. Potier

Water Science & Technology 70 (10), 1575-84

ABSTRACT

To date, computational fluid dynamics (CFD) models have been primarily used for evaluation of hydraulic problems at wastewater treatment plants (WWTPs). A potentially more powerful use, however, is to simulate integrated physical, chemical and/or biological processes involved in WWTP unit processes on a spatial scale and to use the gathered knowledge to accelerate improvement in plant models for everyday use, that is, design and optimized operation. Evolving improvements in computer speed and memory and improved software for implementing CFD, as well as for integrated processes, has allowed for broader usage of this tool for understanding, troubleshooting, and optimal design of WWTP unit processes. This paper proposes a protocol for an alternative use of CFD in process modelling, as a way to gain insight into complex systems leading to improved modelling approaches used in combination with the IWA activated sludge models and other kinetic models.

Key words | biokinetic models, CFD, complex systems, fluid motion, multi-phase flow, transport models

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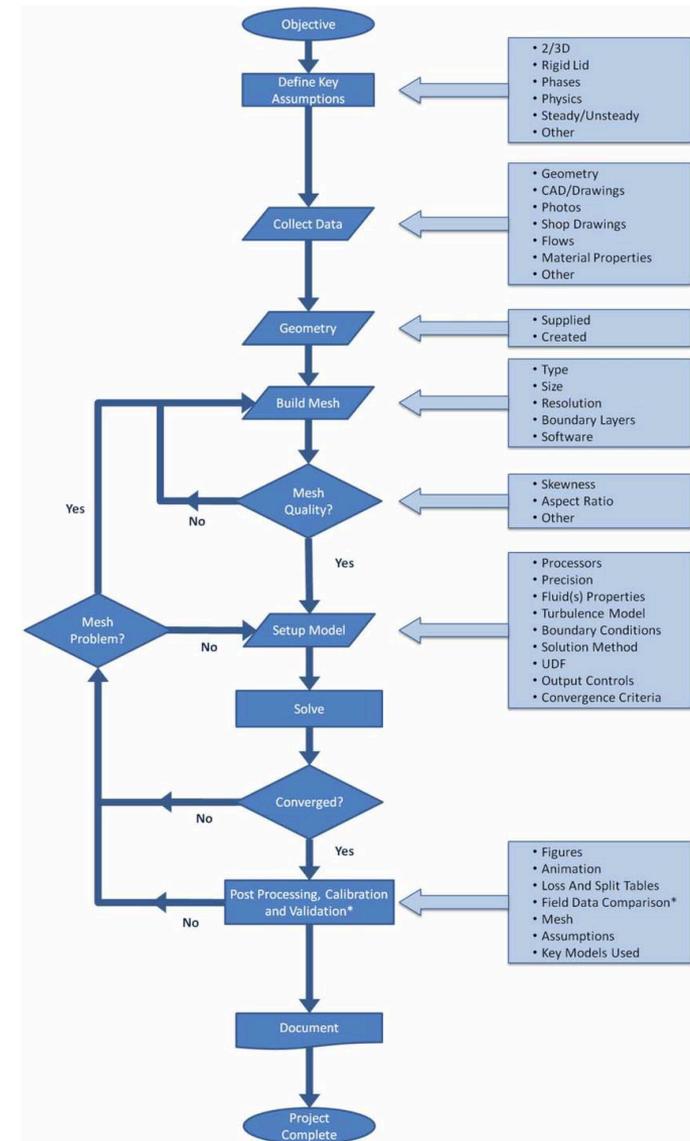
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Edward Wicklein, Damien J. Batstone, Joel Ducoste, Julien Laurent, Alonso Griborio, Jim Wicks, Stephen Saunders, Randal Samstag, Olivier Potier and Ingmar Nopens

Complete flow of a CFD modelling process

Good modelling practice in applying computational fluid dynamics for WWTP modelling

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Coming soon...

- CFD for Wastewater Treatment: An Overview
- Scientific & Technical Report
- Student book

Being aware it is only modeling

We try for being close to the reality with the simplest models,

but not the more simplistic ones.

Merci de votre attention !

Gràcies per la seva atenció!